

# Chapter 2

## Temperature Effects in Semiconductors

The changes in temperature described in the previous chapter affect the speed, power, and reliability of our systems. Throughout this book, we will examine all three of these metrics, though the majority of our discussion will be on how temperature affects the speed performance. In this chapter, we discuss the problem of temperature variation at the device and circuit level. In Sect. 2.1, we provide a background on the material dependences on temperature. In Sect. 2.2, the normal and reverse temperature dependence regimes are described. In Sect. 2.3, we explore how these dependences change with technology scaling and the introduction of new processing materials, such as high- $\kappa$  dielectrics and metal gates.

### 2.1 Material Temperature Dependences

In this section we provide details about the impact of temperature on the MOSFET energy band gap, carrier density, mobility, carrier diffusion, velocity saturation, current density, threshold voltage, leakage current, interconnect resistance, and electromigration.

#### 2.1.1 Energy Band Gap

Temperature affects the properties of electronic systems in a number of fundamental ways. The most fundamental of properties is the energy band gap,  $E_g$ , which is affected by temperature according to the Varshni equation [1]

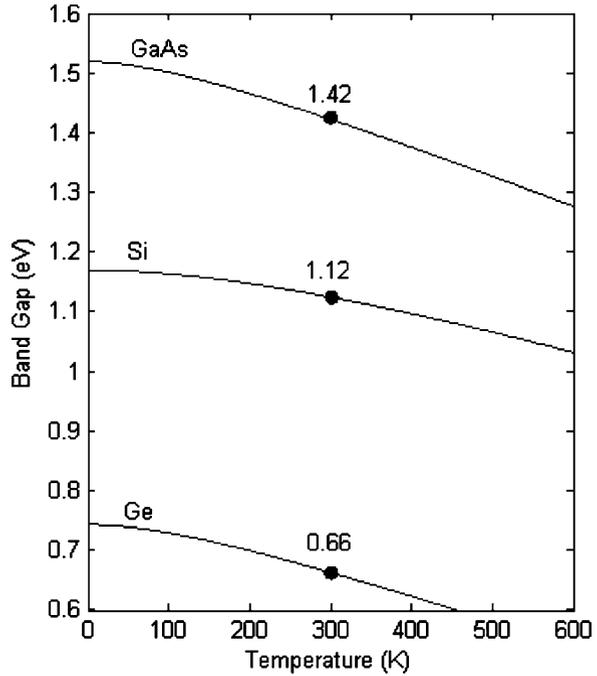
$$E_g(T) = E_g(0) - \frac{\alpha_E T^2}{T + \beta_E} \quad (2.1)$$

where  $E_g(0)$  is the band gap energy at absolute zero on the Kelvin scale in the given material, and  $\alpha_E$  and  $\beta_E$  are material-specific constants. Table 2.1 [2] provides these

**Table 2.1** Varshni equation constants for GaAs, Si, and Ge [2]

Material	$E_g(0)$ (eV)	$\alpha_E$ (eV/K)	$\beta_E$ (K)
GaAs	1.519	$5.41 \cdot 10^{-4}$	204
Si	1.170	$4.73 \cdot 10^{-4}$	636
Ge	0.7437	$4.77 \cdot 10^{-4}$	235

**Fig. 2.1** Energy band gap temperature dependence of GaAs, Si, and Ge



constants for three material structures. Table 2.1 and (2.1) are used to generate Fig. 2.1, which shows how the band gaps of the three materials decrease as temperature increases (the labeled points are the band gap of each material at room temperature).

### 2.1.2 Carrier Density

Carrier densities affect electrical and thermal conductivity, and are a function of the effective density of states in the appropriate band (conduction for n-type, valence for p-type), the Fermi energy level in the material (which is a function of temperature and dopant concentrations), and the temperature as given by the following equations:

$$n = N_C e^{-\frac{E_C - E_F}{kT}} \quad (2.2)$$

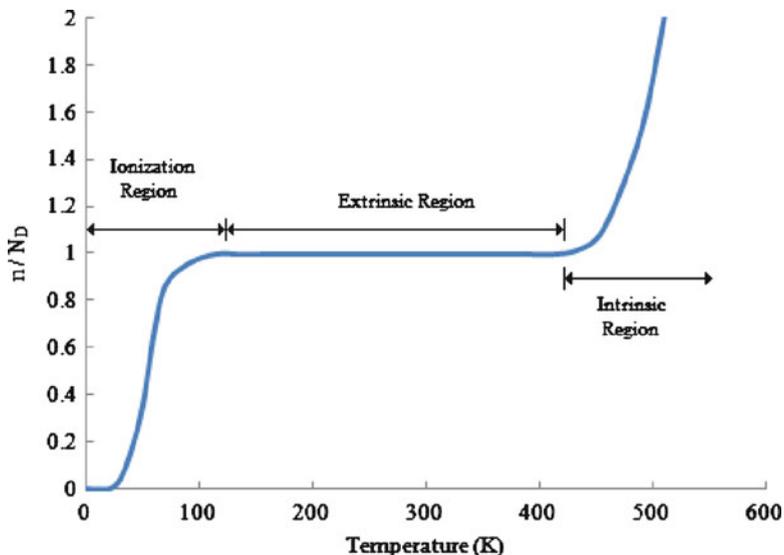


Fig. 2.2 Temperature dependence of  $n$  in a doped semiconductor

$$p = N_V e^{-\frac{E_F - E_V}{kT}} \quad (2.3)$$

where  $n$  is the electron density,  $p$  is the hole density,  $N_C$  is the density of states in the conduction band,  $N_V$  is the density of states in the valence band,  $E_C$  is the conduction band energy level,  $E_V$  is the valence band energy level,  $E_F$  is the Fermi energy level,  $k = 1.38 \cdot 10^{-23}$  J/K is the Boltzmann constant, and  $T$  is temperature.

The temperature dependence of carrier density is shown in Fig. 2.2 for a doped material. In the ionization region, there is only enough latent energy in the material to push a few of the dopant carriers into the conduction band. In the extrinsic region, which is the desired region of operation, the carrier concentration is flat over a wide range of temperatures; in this region, all of the dopant carriers have been energized into the conduction band (i.e.  $n \approx N_D$ ) and there is very little thermal generation of additional carriers. As the temperature increases, the extrinsic region turns into the intrinsic region, and the number of thermally generated carriers exceeds the number of donor carriers. The intrinsic carrier concentration in a material  $n_i$  is generally much smaller than the dopant carrier concentration at room temperature, but  $n_i (=n \cdot p)$  has a very strong temperature dependence [2]

$$n_i \propto T^{1.5} e^{-\frac{E_{g0}}{2kT}} \quad (2.4)$$

where  $E_{g0}$  is the energy band gap at  $T = 0$  K. Depending upon the dopant concentration, the number of thermally generated carriers can exceed the number of dopant-generated carriers, increasing the potential for thermal variation problems.

### 2.1.3 Mobility

We pay particular attention to the temperature and electric field dependence of mobility, as mobility is one of the two main factors (the other is threshold voltage) resulting in the MOSFET temperature behavior shown later in this chapter. The carrier mobility,  $\mu$  ( $\text{cm}^2/\text{V}\cdot\text{s}$ ), describes the drift velocity of a particle in an applied electric field. Under small to moderate electric fields,  $\mu = v_d/\xi$  where  $v_d$  is the drift velocity, and  $\xi$  is the electric field. MOSFET mobility has very complex temperature dependence, defined by the interplay of the following four scattering parameters: phonon scattering  $\mu_{ph}$ , surface roughness scattering  $\mu_{sr}$ , bulk charge Coulombic scattering  $\mu_{cb}$ , and interface charge Coulombic scattering  $\mu_{int}$  [3]. Each of these scattering parameters is related to the temperature of the material,  $T$ , and the effective transverse electric field in the channel,  $\xi_{eff}$ , which is approximated as [4, 5]

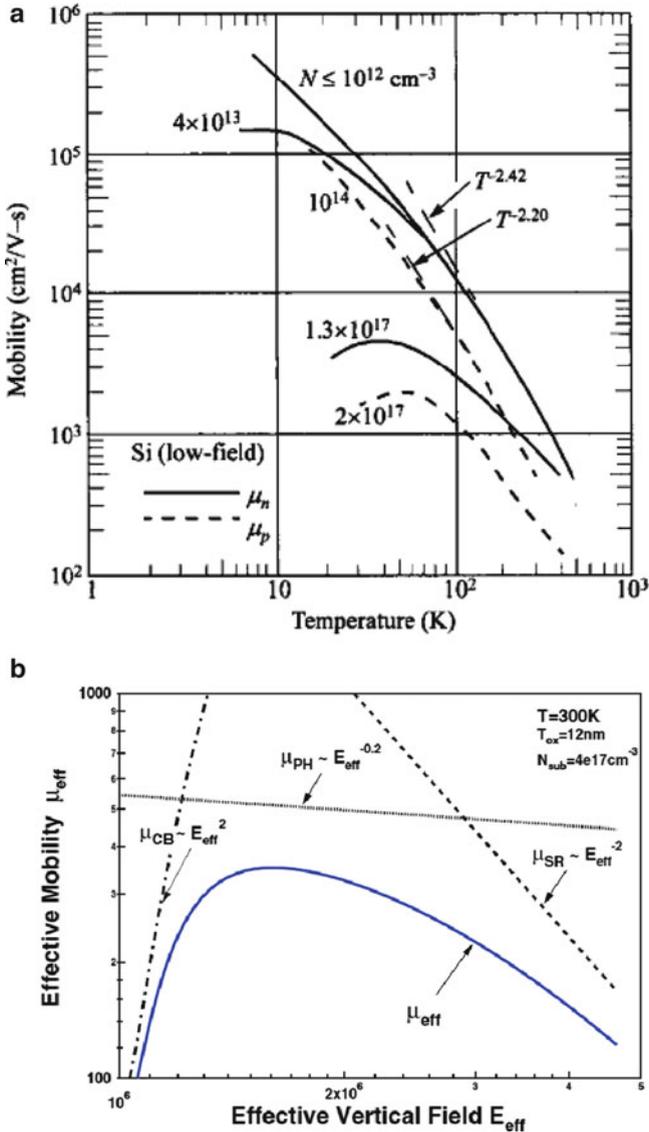
$$\xi_{eff} \approx \frac{(\eta Q_{inv} + Q_b)}{\epsilon_{Si}} \approx \frac{(V_{gs} + V_T)}{6T_{ox}} \quad (2.5)$$

where  $\eta$  is a constant ( $\eta \approx 0.4$  in PMOS devices and  $\eta \approx 0.5$  in NMOS devices),  $Q_{inv}$  is the inversion layer charge density,  $Q_b$  is the substrate depletion charge density, and  $\epsilon_{Si} = 11.7$  is the relative permittivity of Silicon. This approximation is not very convenient for circuit analysis, so  $\xi_{eff}$  is also approximated in terms of the gate-source voltage  $V_{gs}$ , the threshold voltage  $V_T$ , and gate oxide thickness  $T_{ox}$ .

The Berkeley Short-Channel IGFET Model (BSIM), one of the most widely used simulation models, combines these four scattering parameters into an effective mobility,  $\mu_{eff}$  [3] using Matthiessen's rule

$$\frac{1}{\mu_{eff}(T, E_{eff})} \propto \frac{1}{\mu_{ph}(T, E_{eff})} + \frac{1}{\mu_{sr}(T, E_{eff})} + \frac{1}{\mu_{cb}(T, E_{eff})} + \frac{1}{\mu_{int}(T, E_{eff})} \quad (2.6)$$

Phonon scattering refers to the potential for an electron to be scattered by a lattice vibration. As temperature increases, lattice vibrations increase and the probability of an electron being scattered by the lattice increases; thus, high temperature mobilities are limited by phonon scattering ( $\mu_{ph} \propto T^{-3/2}$ ), causing mobility to decrease as temperature increases as shown in Fig. 2.3a. Surface roughness scattering becomes dominant when high electric fields pull electrons closer to the Si/SiO<sub>2</sub> surface ( $\mu_{sr} \propto \xi_{eff}^{-2.1}$ ).



**Fig. 2.3** (a) Temperature dependence of electron and hole mobilities in Si for different dopant concentrations [2], (b) Field dependence of mobility [7]

At low temperatures, electrons move more slowly, and lattice vibrations are small as well; thus, the ion impurity forces which have little impact on high-energy particles become the dominant limit to mobility. In this regime, decreasing temperature extends the amount of time electrons spend passing an impurity ion, causing mobility to decrease as temperature decreases ( $\mu_{cb} \propto T$ ). This effect is emphasized

in the high dopant concentration curves shown in Fig. 2.3a, where mobility decreases with decreasing temperature (e.g. the  $\mu_n = 1.3 \cdot 10^{17}$  dopant concentration line below  $\sim 30$  K).

The electric field dependence of mobility is shown in Fig. 2.3b. In bulk Coulombic scattering, increasing  $\xi_{eff}$  increases the charge density in the channel; the associated charge screening reduces the impact of  $\mu_{cb}$  ( $\propto \xi_{eff}^2$ ). At low temperatures, the interface charges have two conflicting dependences. Reduced temperature reduces the carriers' thermal velocity, which increases the impact of interface charges; however, the reduced thermal velocity also reduces the screening effect [6], and this reduction in screening dominates the temperature dependence ( $\mu_{int} \propto T^{-1}$ ). The electric field screening effect is also weakened by the reduced thermal velocity ( $\mu_{int} \propto \xi_{eff}$ , not  $\xi_{eff}^2$  as in the  $\mu_{cb}$  limit). In this book, we consider devices operating in the phonon scattering limit, with temperatures  $> 200$  K; thus, mobility will decrease as temperature increases.

The temperature dependence of mobility plays a major role in temperature-aware system design, and is discussed in more detail in the next subsection. In room temperature Si, the electron mobility,  $\mu_n$ , is nearly three times as large as the hole mobility,  $\mu_p$ , with  $\mu_n = 1,350 \text{ cm}^2/\text{V}\cdot\text{s}$  and  $\mu_p = 480 \text{ cm}^2/\text{V}\cdot\text{s}$ .

### 2.1.4 Carrier Diffusion

Diffusion is the movement of particles from a region of high concentration to a region of low concentration. Carrier diffusion coefficients  $D_n$  and  $D_p$  (for electrons and holes, respectively) are related to mobility by the Einstein relationship

$$\frac{D}{\mu} = \frac{kT}{q} \quad (2.7)$$

Here,  $q$  is the charge on an electron ( $1.6 \cdot 10^{-19}$  C), and  $kT/q$  is an important value known as the thermal voltage,  $\phi_T$ . At room temperature (300 K),  $\phi_T = 0.0259$  V.  $D_n$  and  $D_p$  in room temperature silicon are 36 and  $12 \text{ cm}^2/\text{s}$ , respectively.

### 2.1.5 Velocity Saturation

Although saturation velocity has been recently found to be a dominant temperature-dependent parameter, notable work had been performed in this area as far back as 1970 [8] using device lengths of  $10 \text{ }\mu\text{m}$ . In the BSIM4 device model, the impact of temperature on velocity saturation  $v_{sat}$  is modeled by [9]

$$v_{sat} = v_{sat0} \cdot [1 - \alpha_{v_{sat}}(T - T_0)] \quad (2.8)$$

where  $v_{sat0}$  is the saturation velocity at nominal temperature ( $T_0$ ) and  $\alpha_{v_{sat}}$  is the saturation velocity temperature coefficient. Qualitatively, velocity saturation is the point at which increases in energy no longer cause carrier velocity to increase; instead, the additional energy is lost to phonon generation through lattice interactions.

In the results presented in this book, devices operate in the velocity saturation regime; thus, the impact of temperature on saturation velocity (increasing temperature decreases  $v_{sat}$ ) is one of the most important criteria affecting the overall impact of temperature on device current, as will be shown later in this chapter.

### 2.1.6 Current Density

The temperature dependence of the carrier concentrations, mobilities and diffusion coefficients affect the temperature behavior of the carrier current densities, with the carrier densities defined by the following formulas [10]:

$$J_N = q\mu_n n \xi + qD_n \nabla n \quad (2.9)$$

$$J_P = q\mu_p p \xi - qD_p \nabla p \quad (2.10)$$

where  $J_N$  and  $J_P$  are the electron and hole current densities, respectively. The first term in each equation is the *drift* component of the total current, with  $\mu_n$  and  $\mu_p$  corresponding to the electron and hole mobilities, respectively;  $\xi$  is the electric field. The second term in each equation is the *diffusion* component of the total current, with  $\nabla n$  and  $\nabla p$  corresponding to the electron and hole concentration gradients (if there is no concentration gradient, there is no diffusion). The temperature dependent parameter in the second term is the diffusion coefficient. Increased temperature increases particle kinetic energy, increasing the diffusion component of total current. The drift component of the total current has two temperature dependent parameters, the mobility and the carrier density. The mobility term was shown in Fig. 2.3 to decrease as temperature increases (in the lattice vibration-limited case) while the carrier density remains nearly fixed with temperature over the extrinsic range (our intended range of operation), as indicated by Fig. 2.2. Thus, we determine that the drift component of the total current decreases as temperature increases.

The drift and diffusion currents have opposing temperature dependencies, which causes the net current change to depend on the applied electric field. In the high-field (drift-dominated) case, current decreases as temperature increases; in the low-field (diffusion-dominated) case, current increases as temperature increases. However, if the system in question is a multi-voltage system, and the system has both drift- *and* diffusion-dominated components, the impact of temperature variation may become less well-defined. The difference between a drift-dominated system and a diffusion-dominated system is defined by the threshold voltage,  $V_T$ . We will show that the temperature dependences of mobility and threshold voltage result in some very interesting device behavior.

### 2.1.7 Threshold Voltage

The MOSFET threshold voltage is given by [2]

$$V_T = V_{FB} + 2\phi_F + \gamma\sqrt{2\phi_F} \quad (2.11)$$

where  $V_{FB} = \phi_{gs} - (Q_{ss}/C_{ox})$  is the flat band voltage, with the gate-substrate contact potential  $\phi_{gs} = \phi_T \ln(N_A N_G / n_i^2)$ ,  $N_A$  and  $N_G$  are the substrate and gate doping concentrations, respectively,  $Q_{ss}$  the surface charge density, and  $C_{ox}$  the oxide capacitance;  $\gamma = C_{ox}(2q\epsilon_{Si}N_A)^{0.5}$  is a body effect parameter, with  $\epsilon_{Si}$  the relative permittivity of Si;  $\phi_F = \phi_T \ln(N_A/n_i)$  is the Fermi energy with the thermal voltage  $\phi_T = kT/q$ , and  $n_i$  the intrinsic carrier concentration of Si.

Of the parameters in (2.11),  $\phi_{gs}$  and  $\phi_F$  vary with temperature (each contains  $\phi_T$  and  $n_i$  terms). The threshold voltage temperature dependence  $\partial V_T / \partial T$  may thus be written as [11]

$$\frac{\partial V_T}{\partial T} = \frac{\partial \phi_{gs}}{\partial T} + 2 \frac{\partial \phi_F}{\partial T} + \frac{\gamma}{\sqrt{2\phi_F}} \frac{\partial \phi_F}{\partial T} \quad (2.12)$$

where the temperature dependencies of  $\phi_{gs}$  and  $\phi_F$  are [11]

$$\frac{\partial \phi_{gs}}{\partial T} = \frac{1}{T} \left( \phi_{gs} + \frac{E_{G0}}{q} + \frac{3kT}{q} \right) \quad (2.13)$$

$$\frac{\partial \phi_F}{\partial T} = \frac{1}{T} \left[ \phi_F - \left( \frac{E_{G0}}{2q} + \frac{3kT}{2q} \right) \right] \quad (2.14)$$

Filanovsky [11] used empirical parameters from a 0.35  $\mu\text{m}$  CMOS technology to determine that the three terms in (2.12) are  $-3.1$ ,  $2.7$ , and  $-0.43$  mV/K, resulting in a net threshold temperature coefficient of  $-0.83$  mV/K. The threshold voltage in a MOSFET is commonly modeled to decrease linearly with increasing temperature; the parameter is plotted in Fig. 2.4 over a range of oxide thicknesses  $d$  and dopant concentrations  $N_A$ .

### 2.1.8 Leakage Current

Subthreshold leakage current  $I_{sub}$  is exponentially dependent on temperature, as shown in Fig. 2.5; a common rule of thumb is that leakage current doubles for every  $10^\circ\text{C}$  increase in temperature [12]. When  $V_{GS} = 0$ ,  $I_{sub}$  may be represented by the Shockley diode model

$$I_{sub} = I_0 \left( e^{\frac{V_{DS}}{\phi_T}} - 1 \right) \quad (2.15)$$

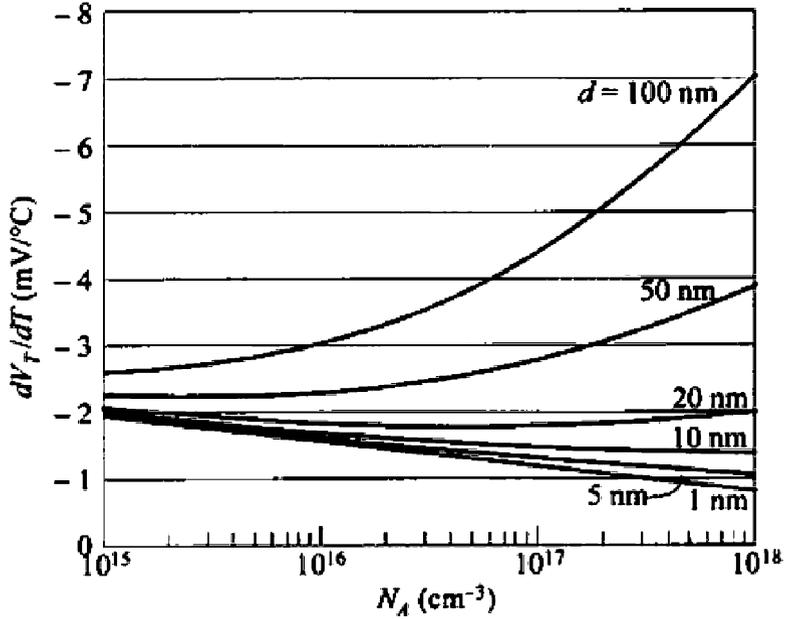


Fig. 2.4 Change in threshold voltage temperature dependence at room temperature vs. dopant concentration, with oxide thickness  $d$  [2]

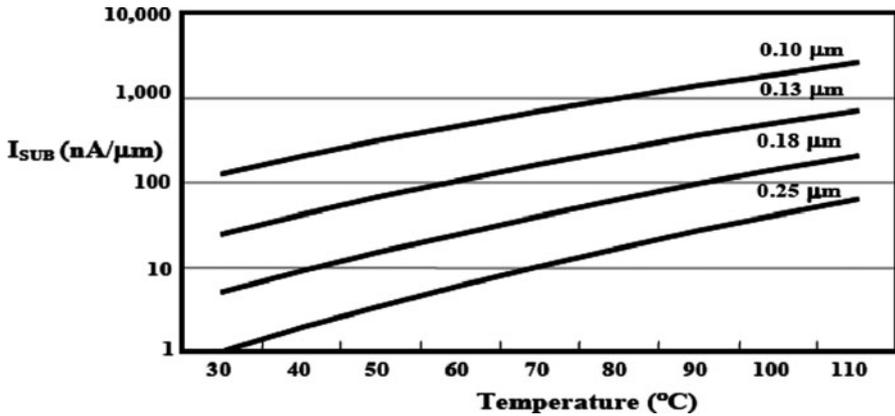


Fig. 2.5 Temperature dependence of subthreshold leakage current ( $V_{GS} = 0$  V) [14]

$$I_0 = ATe^{-\frac{1.12}{2\phi_T}} \tag{2.16}$$

where  $I_0$  is the reverse saturation current [12],  $A$  is a constant, and  $V_{DS}$  is the drain-source voltage. Recalling that  $\phi_T = kT/q$ , we see that  $I_0$  is responsible for the exponential temperature dependence shown in Fig. 2.5.

The temperature dependence of gate leakage current has been shown to be very minor compared to that of subthreshold leakage current [13].

### 2.1.9 Interconnect Resistance

The interconnect resistance  $R$  is related to temperature by

$$R(T) = R_0[1 + \alpha_R(T - T_0)] \quad (2.17)$$

where  $T$  is the temperature,  $R_0$  is the resistance at nominal temperature  $T_0$ , and  $\alpha_R$  is an empirical term named the temperature coefficient of resistance. Al and Cu interconnects have similar values of  $\alpha_R$ —0.004308 and 0.00401, respectively. Over the military-specified temperature range, Al wire resistances can change by up to 77.5% while Cu wire resistances can change by up to 72.2%. Interconnect resistance increases with increasing temperature, complicating evaluation of the impact of temperature on interconnect links—in these applications, the MOSFET currents may either increase or decrease in temperature (as explored in the next subsection), which means that the impact of temperature on interconnect resistance can either add to the system temperature dependence or reduce the temperature dependence, depending on the operating conditions.

### 2.1.10 Electromigration

Electromigration is a failure mechanism caused by high-energy electrons impacting the atoms in a material and causing them to shift position. It is most problematic in areas of high current density. This can form a positive feedback path where electromigration will cause an atom to move down a wire, slightly narrowing the wire width at that location and increasing the current density; this increased current density then further increases electromigration, causing more atoms to be displaced. This brings about two failure mechanisms: (1) the narrowing of the wire will increase wire resistance, which may cause a timing failure if a signal can no longer propagate within the clock period, or (2) electromigration will continue until the wire completely breaks, allowing no further current flow and resulting in functional failure.

Electromigration's impact on a system's reliability is measured in terms of a mean time to failure (MTTF) using Black's equation [15]

$$MTTF = A_j \cdot J^{-n_j} \cdot e^{\frac{E_a}{kT}} \quad (2.18)$$

where  $A_j$  is a constant related to the cross-sectional area of a wire,  $J$  is the current density,  $n$  is a constant scaling factor,  $E_a$  is the activation energy,  $k$  is the Boltzmann constant, and  $T$  is temperature. Thus, the MTTF is exponentially dependent on temperature.

## 2.2 Normal and Reverse Temperature Dependence

Changes in temperature affect system speed, power, and reliability by altering the threshold voltage [11], mobility [11], and saturation velocity [16] in each device. The resulting changes in device current can lead to failures in timing, cause systems to exceed power or energy budgets, and result in communication errors between IP cores. The temperature relationships for MOSFET mobility, threshold voltage, and velocity saturation are related to temperature using the following empirical expressions [17]:

$$\mu(T) = \mu_0(T/T_0)^{\alpha_\mu} \quad (2.19)$$

$$V_T(T) = V_{T0} + \alpha_{V_T}(T - T_0) \quad (2.20)$$

$$v_{sat}(T) = v_{sat0} + \alpha_{v_{sat}}(T - T_0) \quad (2.21)$$

where  $T$  is the temperature;  $T_0$  is the nominal temperature;  $\mu_0$ ,  $V_{T0}$ , and  $v_{sat0}$  are the mobility, threshold voltage, and saturation velocity at  $T_0$ , respectively;  $\alpha_\mu$ ,  $\alpha_{V_T}$ , and  $\alpha_{v_{sat}}$  are empirical parameters named the mobility temperature exponent, threshold voltage temperature coefficient, and saturation velocity temperature coefficient, respectively, where  $\alpha_\mu \approx -1.3$ ,  $\alpha_{V_T} \approx -3$  mV/°C, and  $\alpha_{v_{sat}} \approx -97$  m/(s·°C). Two temperature dependencies exist: the normal dependence (ND) region, where drain current ( $I_D$ ) *decreases* with increasing temperature, and the reverse dependence (RD) region, where  $I_D$  *increases* with increasing temperature [18]. Between the two regions, there is a supply voltage where the impact of temperature on delay is minimized. This is referred to as the temperature-insensitive voltage  $V_{INS}$  [19], and as technology scales this voltage approaches nominal voltage.

In the temperature region of concern (between  $-55^\circ\text{C}$  and  $125^\circ\text{C}$ , the range of military operating temperatures [20]),  $\mu$ ,  $V_T$ , and  $v_{sat}$  all decrease with increasing temperature. Examining the velocity-saturated MOSFET drain current  $I_D(T)$  [21] we see that decreasing  $v_{sat}$  *decreases*  $I_D$ , while decreasing  $V_T$  *increases*  $I_D$  [22].

$$I_D(T) = v_{sat}(T) \cdot W \cdot P_s \cdot [V_{GS} - V_T(T)]^\alpha \quad (2.22)$$

Where  $W$  is the device width,  $P_s$  is a technology-specific constant,  $V_{GS}$  is the MOSFET gate-source voltage, and  $\alpha$  is a technology-specific exponent. The temperature dependence of the MOSFET drain current,  $dI_D/dT$ , can be determined by the sum of the impacts of  $v_{sat}$  and  $V_T$  on  $I_D$ , composed of four values—(1) the change in velocity

saturation for a change in temperature,  $dv_{sat}/dT$ , (2) the change in threshold voltage for a change in temperature,  $dV_T/dT$ , (3) the change in device current for a change in velocity saturation,  $\partial I_D/\partial v_{sat}$ , and (4) the change in device current for a change in threshold voltage,  $\partial I_D/\partial V_T$ :

$$\left. \frac{dI_D}{dT} \right|_{Tot} = \left. \frac{dI_D}{dT} \right|_{v_{sat}} + \left. \frac{dI_D}{dT} \right|_{V_T} = \frac{\partial I_D}{\partial v_{sat}} \cdot \frac{dv_{sat}}{dT} + \frac{\partial I_D}{\partial V_T} \cdot \frac{dV_T}{dT} \quad (2.23)$$

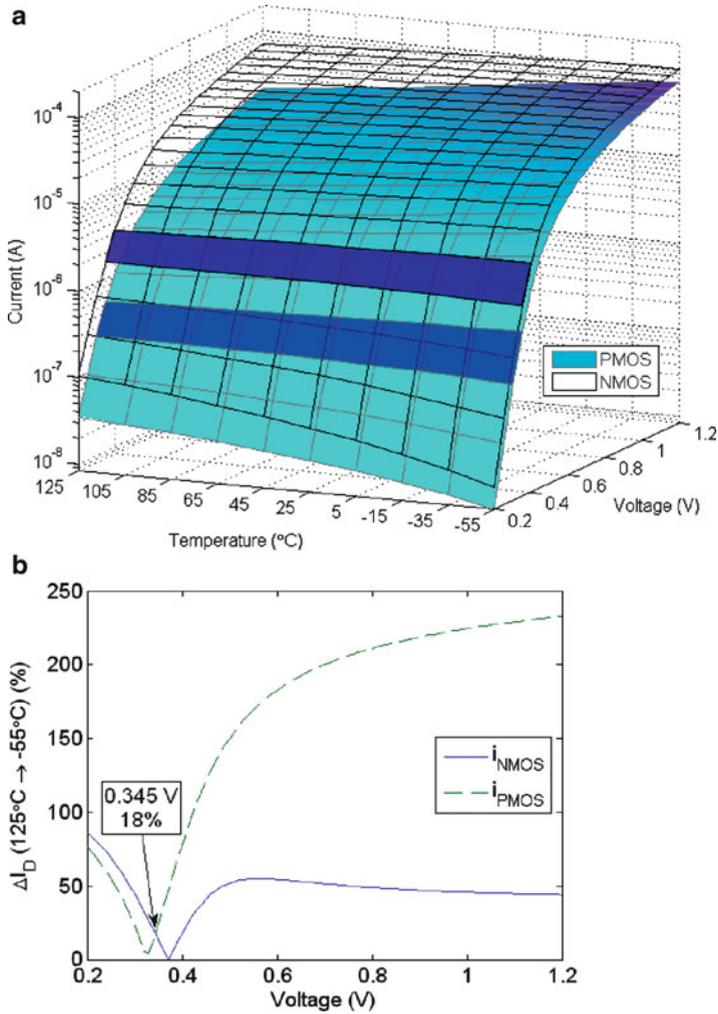
$dI_D/dT|_{v_{sat}}$  is negative, and  $dI_D/dT|_{V_T}$  is positive. At nominal voltage in conventional CMOS technologies, the magnitude of  $dI_D/dT|_{v_{sat}}$  is greater than the magnitude of  $dI_D/dT|_{V_T}$ ; thus, circuits at nominal voltages become slower as temperature increases. However, as  $V_{GS}$  approaches  $V_T$ , a change in  $V_T$  has a larger impact on  $I_D$ ; thus, at lower supply voltages, the magnitude of  $dI_D/dT|_{v_{sat}}$  is less than the magnitude of  $dI_D/dT|_{V_T}$ , and device delay decreases as temperature increases (the reverse temperature dependence).  $V_{INS}$  occurs where  $dI_D/dT|_{Tot}$  approaches zero, with  $dI_D/dT|_{v_{sat}} \approx -dI_D/dT|_{V_T}$ ; however, because  $v_{sat}$  and  $V_T$  differ between NMOS and PMOS devices, each type of device has a different value of  $V_{INS}$ . The dependence regions are shown in Fig. 2.6 for plots of the current through diode-connected PMOS and NMOS devices in a 90 nm technology model [23] over the range of military operating temperatures. In Fig. 2.6a,  $V_{INS}$  occurs in the shaded regions, with higher voltages exhibiting the normal temperature dependence and lower voltages exhibiting the reverse temperature dependence.

The reverse temperature dependence is occasionally referred to as temperature inversion, while the normal and reverse temperature dependences are also referred to as negative (for normal dependence) and positive (for reverse dependence) current-temperature ( $I$ - $T$ ) slopes. In this document, we will use the  $\pm I$ - $T$  slope terminology as shorthand for the normal and reverse temperature dependences.

The difference between the 125°C and -55°C endpoints of Fig. 2.6a is presented in Fig. 2.6b. In Fig. 2.6b,  $V_{INS}$  is indicated in each device by the minimum points in each curve; the absolute minimum for a 1:1 sizing ratio occurs at 345 mV, corresponding to an 18% total change in current over the entire 180°C range of ambient temperatures.

### 2.2.1 *Discovery of the Normal and Reverse Temperature Dependences*

This book is by no means the first document to report on the reverse temperature dependence. Indeed, what we name the reverse temperature dependence (i.e. the increasing of electrical conduction with increasing temperature) was first discovered by Faraday with his silver sulphide experiments mentioned in the previous chapter. However, the mechanism detected by Faraday was quite different than the



**Fig. 2.6** (a) Device current across a range of temperatures and supply voltages in a 90 nm technology, (b) temperature change from 125 $^{\circ}\text{C}$  to -55 $^{\circ}\text{C}$

mechanisms causing the normal and reverse temperature dependences in our modern Silicon electronics. The first recorded mention of the reversal of the temperature dependence describing the trade-off between mobility and threshold voltage is attributed to C. Park, *et al.*, from Motorola in 1995, in a conference paper exploring the impact of temperature on integrated circuits at very low voltages [18]. In the time since, the reversal of the temperature dependence has been explored in great detail [11, 24, 25], including magazines, patents, and journal papers, and is now being considered in industry-standard tools [26].

### 2.3 Temperature and Technology Scaling

$V_{INS}$  occurs at increasingly larger supply voltages as technology is scaled, and is fast approaching the nominal supply voltage  $V_{NOM}$  (which is steadily decreasing as technology scales) as shown in Table 2.2, particularly with the introduction of high- $\kappa$  dielectrics to replace  $\text{SiO}_2$  [27] (high- $\kappa$  dielectrics reduce  $\mu$  and change  $\partial\mu/\partial T$  [28], altering the balance of the  $\mu$  and  $V_T$  impacts). The change in  $V_{INS}$  as technology scales is caused by changes in the threshold voltage and saturation velocity [29]. The data in Table 2.2 were generated using predictive technology models [23], with the 45, 32, and 22 nm data points using high- $\kappa$  dielectric/metal gate models.

As  $V_{INS}$  approaches  $V_{NOM}$ , adaptive systems which vary supply voltage to reduce energy consumption or improve reliability will have operating voltages in both the normal and reverse temperature dependence regions, making it unclear if circuits will increase in speed or decrease in speed as chip temperatures increase, and exacerbating problems associated with inter-die temperature variation; solutions to this issue are discussed in Chap. 3.

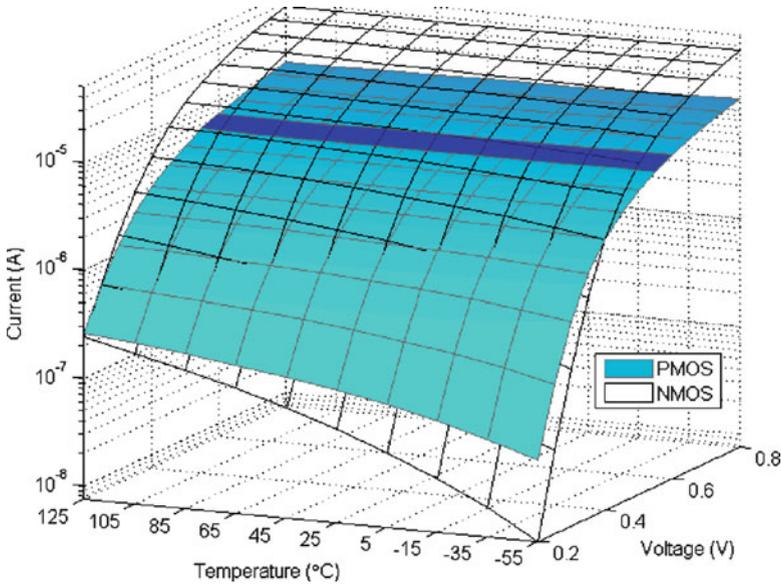
The current dependencies for a 22 nm technology with high- $\kappa$  dielectrics and metal gates are shown in Fig. 2.7. As shown,  $V_{INS}$  in the PMOS device increases from  $\sim 375$  mV at 90 nm to  $\sim 575$  mV at 22 nm, with the nominal supply voltage decreasing from 1.2 V at 90 nm to 0.8 V at 22 nm. The 22 nm NMOS device is in the reverse temperature dependence region even at the nominal supply voltage.

#### 2.3.1 The Reverse Temperature Effect and High- $\kappa$ /Metal Gate Technology

$V_T$ ,  $\mu$ ,  $v_{sat}$  and nominal supply voltage are all technology dependent parameters, with predicted values available down to the 22 nm node [23, 30]. Use of high- $\kappa$  dielectrics and metal gates to alleviate nanoscale gate leakage problems also alters  $V_T$ ,  $\mu$ , and  $v_{sat}$  [31, 32]. The combination of these changes makes it difficult to determine the effect of temperature on device performance. Two dependences exist, as mentioned in the prior subsection: a normal temperature dependence, where current decreases as temperature increases, and a reverse temperature dependence [18, 19], where current increases as temperature increases.

**Table 2.2**  $V_{INS}$  approaches  $V_{NOM}$  as technology scales

Technology (nm)	$V_{NOM}$ (V)	$V_{INS}$ (V)	$V_{INS}/V_{NOM}$
90	1.2	0.39	0.33
65	1.1	0.40	0.36
45	1.0	0.61	0.61
32	0.9	0.69	0.77
22	0.8	0.73	0.91



**Fig. 2.7** Temperature dependence of device current across a range of supply voltages in a 22 nm high- $\kappa$ /metal gate technology

These parameters are further complicated by environmental requirements (military specifications call for a range of  $-55$ – $125^\circ\text{C}$  [20]) and intra-die temperature variation (shown to exceed  $50^\circ\text{C}$  [33]). To account for the wide range of conditions, as well as process and voltage variations, variation-tolerant adaptive systems have been used to guarantee functionality by adjusting operating voltages and frequencies [34–36]; however, these systems with multiple voltage modes make the above-mentioned temperature effects even more difficult to determine.

For large gate overdrives ( $V_{GS}-V_T > V_{INS}$ ), the temperature dependence of a device is dominated by the dependence of  $v_{sat}$ , while for small gate overdrives ( $V_{GS}-V_T < V_{INS}$ ), small changes in  $V_T$  can cause large changes in current, resulting in a temperature dependence dominated by  $V_T$ . Further examination of these effects in  $\text{SiO}_2$  dielectric, polysilicon gate devices is available in [18, 19].

In nanoscale devices, high- $\kappa$  dielectrics and metal gates have been introduced to reduce gate leakage due to thinning gate oxides and reduce the depletion effects of polysilicon gates [31, 32]; unfortunately, these techniques have the effect of dramatically altering the temperature dependence of  $I_D$ . The extent of the change is shown in Fig. 2.8, which compares 45 nm predictive technology models [23] of both  $\text{SiO}_2$ /poly gate (dashed line) and high- $\kappa$ /metal gate (solid line) devices. Each line in Fig. 2.8 shows the change in delay of an inverter (sizing ratio  $\beta = 2$ ) from  $-55^\circ\text{C}$  to  $125^\circ\text{C}$ . For example, at 0.62 V, the high- $\kappa$ /metal gate inverter delay is unchanged from  $-55^\circ\text{C}$  to  $125^\circ\text{C}$ , resulting in the 0.62 V point occurring on the 0% line. This 0% intersect point on each curve represents  $V_{INS}$ . As shown,  $V_{INS}$  in the high- $\kappa$ /metal gate is 40% higher than in the  $\text{SiO}_2$ /poly gate devices.

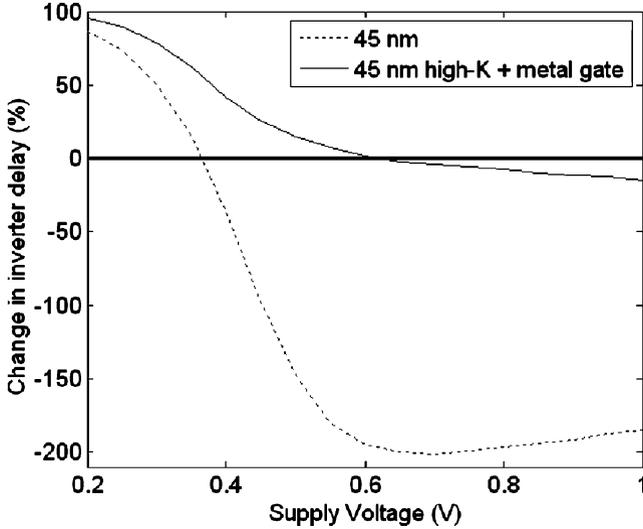


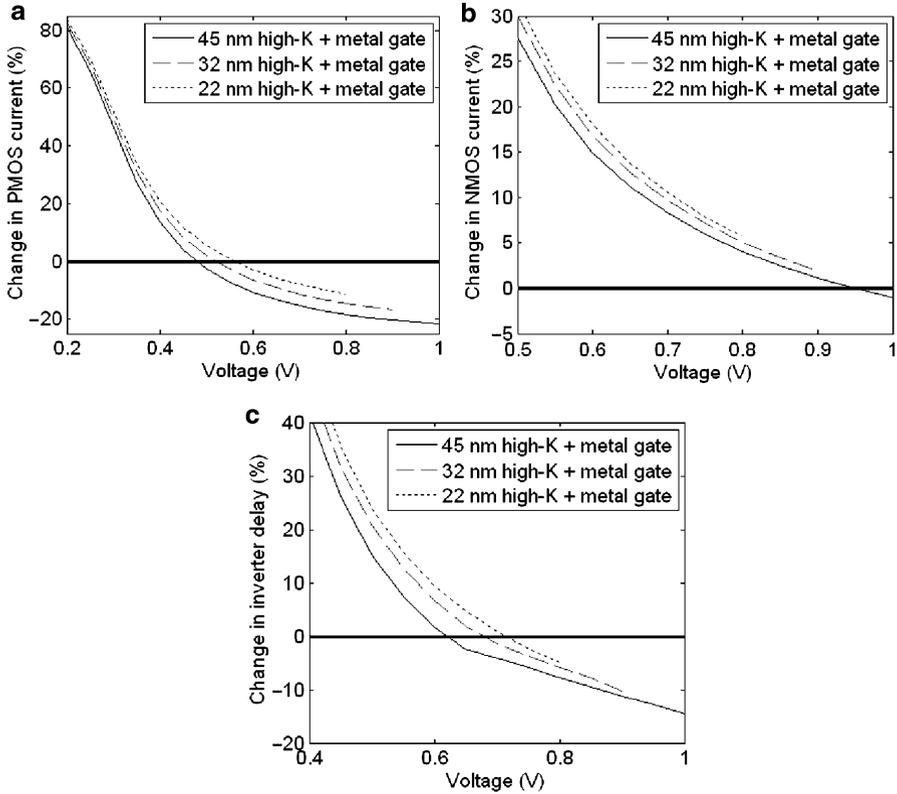
Fig. 2.8 Effect of high- $\kappa$  dielectric and metal gate on temperature dependence

The normal dependence region is below the 0% line, and the reverse dependence region is above the 0% line.

Fig. 2.9a shows the change in PMOS device current from  $-55^{\circ}\text{C}$  to  $125^{\circ}\text{C}$  at the 45, 32, and 22 nm technology nodes (with nominal voltages of 1, 0.9, and 0.8 V, respectively). As shown,  $V_{INS}$  increases by  $\sim 40$  mV per technology node, with  $V_{INS}$  at 22 nm equal to 0.56 V. The NMOS device response, shown in Fig. 2.9b, is in the reverse temperature dependence region over the entire range of operating voltages at the 32 and 22 nm nodes.

The PMOS and NMOS devices are combined into an inverter with  $\beta = 2$  in Fig. 2.9c. As shown,  $V_{INS}$  approaches 90% of nominal voltage in the 22 nm node. As  $\beta$  increases, the stronger PMOS effect decreases  $V_{INS}$ . Thus, adaptive voltage systems may easily wind up straddling both temperature domains in nanoscale systems, making temperature-aware design increasingly critical as technology scales.

Reverse temperature dependence at near nominal voltages complicates variation-tolerant system design, which uses multiple supply voltages to adjust for changes in process, voltage, and temperature. The additional complexity needed to account for both normal and reverse temperature dependence depends on the available design time information. If the system can be fully characterized at design time, then the multiple dependences can be programmed into the voltage and frequency look-up table entries [34] to ensure that the system adapts in the correct direction given a change in temperature. For example, whereas a low-voltage system would generally reduce the frequency as temperature increases, in the reverse dependence region the system would have to reduce the frequency when temperature decreases.



**Fig. 2.9** Changes in (a) PMOS current, (b) NMOS current, and (c) inverter delay over the  $-55^{\circ}\text{C}$  to  $125^{\circ}\text{C}$  temperature range

The reverse temperature effect is particularly important to consider in adaptive systems because of thermal runaway. In the normal dependence region, temperatures are prevented from increasing to dangerous levels because the delay becomes so large that the adaptive system is forced to reduce the clock frequency, reducing the energy and therefore the temperature. In the reverse temperature dependence region, circuits continue to speed up as temperature increases; there is no delay limit on high temperature operation. The higher temperatures could result in thermal runaway resulting from the exponential temperature dependence of leakage current [37], which may already be dominating the total power consumption in the nanoscale regime [38].

If the temperature dependences are not known at design time (from tool limitations, process variations, unknown IR drops, etc.), there are two options to ensure variation-tolerance. The system may be designed with large enough guardbands that it can operate correctly over the entire temperature range regardless of the temperature dependence, though this will result in a large reduction in delay performance. Another option is to use a temperature dependence sensor to determine the temperature dependence at each operating voltage; we propose the first temperature dependence sensor in Chap. 3.

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<http://www.springer.com/978-1-4614-0747-8>

Managing Temperature Effects in Nanoscale Adaptive  
Systems

Wolpert, D.; Ampadu, P.

2012, XXII, 174 p., Hardcover

ISBN: 978-1-4614-0747-8